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FUNCTIONAL SERVICING REPORT

401 CANAL BANK STREET (FORMERLY DAIN CITY COMMUNITY)

CITY OF WELLAND

Prepared by:

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March 2020



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- Overall Watermain Distribution Plan DWG# 0585-FSR WM
- Overall Sanitary Drainage Area Plan DWG# 0585-FSR SAN
- Overall Storm Drainage Area Plan DWG# 0585-FSR STM
- Overall Site Grading Plan DWG# 0585-FSR GP
- Dain City East Draft Plan of Subdivision February 20, 2020
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- Road Section-Utility Locations 23.0m R.O.W.



References

- Design Guidelines for Sewage Works 2008 PIBS 6879 Ontario Ministry of the Environment (2008)
- Existing 2014 Consolidated Regional Official Plan Regional Municipality of Niagara (2014)
- City of Welland Municipal Standards City of Welland (February 2013)
- *Memorandum* "Empire Homes Development Water Distribution System Review" GHD (December 2019)
- Welland City Water and Wastewater Servicing Preliminary Capacity Assessment WSP (March 2020)



EXECUTIVE SUMMARY

Upper Canada Consultants has been retained by Empire Communities to prepare a Functional Servicing Report for the 72.1 hectare, 1405 unit (maximum) development of 401 Canal Bank Street, in the City of Welland.

Water Servicing

A Water Distribution System Review was prepared by GHD for the City of Welland. The GHD study identified that the existing ground elevation within the site would result in water pressures lower than the minimum of 40 psi and provided possible alternatives. The preferred of these alternatives will be to limit the ground elevation to 185.00m, which will result in pressures above the minimum of 40 psi. To service the site, the existing 400mm diameter cast iron watermain shall be redirected and replaced within the site with a new 400mm diameter PVC watermain.

Sanitary Servicing

A sanitary analysis including the Forks Road sanitary sewers and the 450mm diameter trunk sanitary sewer which begins on Crescent Drive and outlets to the Dain City pumping station concluded that the Forks Road sanitary sewers will need to be upgraded to 375mm diameter sewers, but the existing invert elevations and slopes would be adequate to convey peak sanitary flows to the 450mm diameter Crescent Drive sewers.

WSP prepared a study of the existing Welland wastewater infrastructure. The Niagara Region and City of Welland have advised that remediation projects have been undertaken to improve the available capacity at the Dain City pumping station. Following the completion of these projects, the existing infrastructure is expected to have adequate capacity to service the proposed development.

Stormwater Management

Stormwater quality improvements are to be provided to an MECP *Normal* level for stormwater discharging from the site into either the Welland Canal or to the Old Welland Canal. Quantity controls up to the 100 year design storm event have been requested for site stormwater flows discharging to the Welland Canal but are not considered necessary for the Old Welland Canal.

To provide the required MECP *Normal* quality improvement levels prior to discharge into the Welland Canal, a stormwater management wet pond facility is proposed. To provide the requested quantity controls prior to discharge into the Welland Canal, the proposed wet pond facility shall control peak stormwater flows up to the 5 year design storm event and a dry detention facility located will provide quantity controls during major storms exceeding the 5 year design storm. To provide the required quality controls prior to discharging ultimately to the Old Welland Canal, a Hydroworks HG4 oil/grit separator, or approved equivalent is proposed.



INTRODUCTION

This report is to address the servicing needs for the 1,405 unit (maximum), mixed residential development of 401 Canal Bank Street. The site is located within the City of Welland, bound to the east by the Welland Canal, south of the Canadian National Railway lands, north of Forks Road, and east of the former John Deere lands. The site is currently vacant land with an existing hydro corridor located at the northern extent of the site.

The site is 72.1 hectares and shall consist of a maximum of 1,405 units ranging from single detached, semi-detached and town home dwellings as shown in the enclosed Draft Plan of Subdivision. The site shall include associated asphalt roads with a proposed structure of 450mm of Granular 'A' roadway base on finished subgrade, 75mm of HL8 base course asphalt, and 40mm of HL3 surface course asphalt. Additionally, the site shall include concrete curb, catch basins, storm sewers, sanitary sewers, watermain and associated utilities in a joint trench installation. See Appendix A for the proposed 18m, 21m, and 23m internal right of way cross sections.

The development is planned to be phased and constructed starting from south to north to ensure downstream servicing is constructed first, providing the permanent outlets for the following phases.

A study was prepared by WSP regarding the Welland City Water and Wastewater Servicing and should be read in conjunction with this report (WSP, 2020).

The objectives of this study are as follows:

- 1. Identify domestic and fire protection water service needs for the site.
- 2. Identify sanitary servicing needs for the site.
- 3. Provide a summary of the stormwater management plan for the site.
- 4. Provide a summary of the preliminary grading plan for the site.

WATER SERVICING

An analysis of the proposed 401 Canal Bank Street water demand was conducted by GHD for the City of Welland in December of 2019. The study analysed existing and future conditions for the existing infrastructure (the Welland Water Treatment Plant, Bemis Park Elevated Tank, etc.) and concluded that the existing infrastructure could provide adequate domestic and fire supply for the 401 Canal Bank Street development in addition to future development at the former John Deere facility (GHD, 2019).



The GHD study referenced a total future population of 13,173 persons between the future developments (GHD, 2019). The 401 Canal Bank Street (referred to as Dain City Residential) was allocated 2,990 persons. Based on the proposed draft plan, the total population for the 401 Canal Bank Street development would be a maximum of 4,662 persons using the same population density. However, the future development of the former John Deere facility is in a conceptual design stage and does not have a firm number of lots allocated to them. Therefore, GHD's conclusions regarding the capacities of the existing infrastructure remain valid as it pertains to the 401 Canal Bank Street development. Further analysis of the existing infrastructure will be required as part of future draft plan submissions for the future development.

The study prepared by GHD concluded that the existing maximum ground elevation of 189.00m within the development may result in watermain pressures dropping below the minimum 40 psi in specific areas of the site. To ensure adequate watermain pressure is maintained within the entire site, GHD recommended three alternatives:

- Modifying the Welland Water Treatment Plant (WTP) operating procedures,
- Limiting the ground elevation of the site to a maximum of 185.00m,
- Installing a local booster pump station.

The ground elevation within the site will be lowered to generate fill for future developments, therefore, limiting the site to a maximum elevation of 185.00m is the preferred alternative. As shown in the enclosed Overall Site Grading Plan, a maximum elevation of 185.00m has been maintained within the site.

Based on the findings of this study, the following conclusions are offered:

- The existing 400mm diameter watermain is expected to be of sufficient size to meet domestic and fire supply demands.
- The ground elevation within the proposed development will be limited to 185.00m to ensure watermain pressures remain above the minimum 40 psi within the site.
- The existing 400mm diameter cast iron watermain shall be rerouted and replaced within the development with a new 400mm diameter PVC trunk watermain. The proposed trunk watermain shall connect at the intersection of Forks Road and Crescent Drive, route through the development and reconnect at the north western extent of the site. See the enclosed Overall Watermain Distribution Plan for reference.
- The sections of the existing 400mm diameter cast iron watermain where flow has been redirected shall be decommissioned and abandoned per discussions with City of Welland staff.



- The proposed development will be serviced with internal watermain ranging from 150mm to 400mm in diameter.
- Further analysis of the existing infrastructure will need to be undertaken as part of the design for the future John Deere development to ensure there is adequate capacity to accommodate the projected populations.

An Overall Watermain Distribution Plan has been provided with this report for reference.

SANITARY SERVICING

An analysis of the receiving sanitary sewer system has been conducted as part of this servicing report to determine the impact of the proposed development on the system. The scope of the analysis included the entirety of the 1,405 unit (maximum) development as well as the adjacent the 14 existing lots and approved 86 dwelling development fronting the south side of Forks Road. For the analysis, a general density of 3 persons per unit has been used to approximate the total sanitary flows. The Niagara Region Official Plan, Table 4-1, projects a density of 2.40 persons per unit for the City of Welland in 2021 (Niagara Region, 2014).

The City of Welland has provided GIS data, showing the existing sanitary maintenance hole rim elevations and sanitary sewer inverts along Crescent Drive to the Dain City Sewage Pumping Station. The receiving existing 450mm diameter trunk sanitary sewers have been installed at depths ranging from 4.9m and 6.9m below the existing road surface and an overall slope of approximately 0.30% over the 961m run from the intersection of Forks Road and Crescent Drive to the Dain City Sewage Pumping Station. Therefore, the overall trunk sanitary sewer is expected to have adequate capacity to service the proposed development.

Based on the findings of this analysis, the following conclusions are offered:

- The existing 250mm diameter sanitary sewer on Forks Road, east of Crescent Drive has inadequate capacity for the development area of Dain City Community and should be upgraded up to the entrance at Street A.
- The existing 450mm diameter trunk sanitary sewer on Crescent Drive has adequate capacity to convey sanitary flows from the proposed development to the Dain City Sewage Pumping Station.



The above conclusions lead to the following recommendations:

- That the gravity sanitary sewers on Forks Road, east of Crescent Drive be upgraded from 250mm to 375mm diameter sewers up to the entrance at Street A as shown in the enclosed Overall Sanitary Drainage Area Plan. The existing inverts and grade of the existing 250mm diameter sewer are adequate to convey the peak sanitary flows with the upgraded sanitary sewer size.
- That the development area of Dain City Community shall require sanitary sewers from 200mm to 375mm diameter to allow gravity flow throughout the site.

The Overall Sanitary Drainage Area Plan used in this analysis has been provided with this report for reference.

The Welland City Water and Wastewater Servicing Assessment prepared by WSP (WSP, 2020) provides an analysis of the existing sanitary infrastructure within the City of Welland such as the Wasterwater Treatment Plant and the receiving Dain City and Ontario Street Sewage Pumping Stations. Based on the Region of Niagara Wastewater Master Servicing Plan, WSP assessed the existing and future (2041) capacities for the existing infrastructure to determine the impact of the proposed 401 Canal Bank Street development on the overall sanitary system.

The WSP analysis concluded that the existing Wastewater Treatment Plant will operate at under 80% of the total capacity with the 2041 projections, including the proposed development.

Following discussions with the City of Welland and the Niagara Region, the analysis also notes that a separate study prepared by BluePlan Engineering for the City of Welland concluded that the Dain City pumping station is experiencing greater wet weather flows than estimated within the Niagara Region Wastewater Master Servicing Plan, exceeding the ECA firm capacity for the pumping station in a 10 year storm event (WSP, 2020). The Niagara Region is planning "state of good repair upgrades" for the Dain City pumping station and WSP has advised the maximum expected population for the 401 Canal Bank Street development be incorporated with the pumping station upgrades (WSP, 2020). Other efforts proposed by the City of Welland are expected to alleviate the excess of wet weather flows to the Dain City pumping station even further (WSP, 2020).

The referenced BluePlan Engineering study also advises that the increase in sanitary flows from the proposed development does not trigger a requirement for upgrades at the Ontario Street pumping station (WSP, 2020).

Therefore, based on the findings of the WSP study (WSP, 2020), following the upgrades to the Dain City pumping station tentatively planned by the Niagara Region in 2020, there will be adequate capacity in the existing infrastructure to service the proposed development.



Further analysis of the existing infrastructure will need to be undertaken as part of the design for the future John Deere development to ensure there is adequate capacity to accommodate the projected population.

STORMWATER MANAGEMENT

A detailed Stormwater Management Plan has been prepared to address the overall stormwater management strategy for the site and has been submitted along with this Functional Servicing Report. The following shall summarize the findings of this detailed Stormwater Management Plan.

The overall drainage areas for the site convey peak stormwater flows to the Welland Canal and the Old Welland Canal through multiple drainage outlets. Based on the design criteria provided by the MECP and the City of Welland, it is proposed to provide stormwater quality control for site stormwater flows discharging to the Welland Canal. Per discussions with the St. Lawrence Seaway Management Corporation (SLSMC), quantity controls up to the 100 year design storm event have been requested for site stormwater flows discharging to the Welland Canal. Only **quality** controls will be provided for stormwater flows discharging ultimately to the Old Welland Canal, since the peak flows have been reduced to this outlet as a result of the proposed development.

To provide the quality controls required by the City of Welland and MECP and quantity controls requested by the SLSMC, both a wet pond and a dry detention facility are proposed. The wet pond facility will provide a *Normal* level (70% TSS Removal) of stormwater quality control in accordance with MECP guidelines and provide quantity controls up to the 5 year design storm event. For major storms in excess of the 5 year design storm event, stormwater flows shall surcharge from the internal storm sewers and travel overland through the proposed internal roadways to the proposed park land between Streets B and G. Within the park land, a dry detention facility shall provide a controlled outlet for the major storm events. This dry detention facility will only receive stormwater flows during storms in excess of the 5 year design event.

To provide the required quality controls for stormwater discharging from the Forks Road right of way and ultimately to the Old Welland Canal, a Hydroworks HG4 Oil/Grit Separator, or approved equivalent, is proposed to improve stormwater quality levels to MECP *Normal* levels (70% TSS Removal).

An Overall Storm Drainage Area Plan has been provided with this report for reference. Based on the preliminary storm sewer design sheet, the site can be serviced with mainline storm sewers ranging from 300mm to 1650mm in diameter.



PRELIMINARY GRADING PLAN

An Overall Site Grading Plan has been provided with this report to demonstrate the preliminary grading strategy for the 401 Canal Bank Development.

The majority of the site has been graded to create major overland flow paths for the conveyance of stormwater flows to the proposed park lands between Street B and Street G. There are small portions on the southern and northern limits of the site for which an overland flow path cannot be graded to the park areas. Flows conveyed overland within Street C are directed southerly to Forks Road, where they will outlet to the existing ditches along Forks Road. The portion north from Streets R and N have been graded to convey the overland flows to the existing cut-off ditch at the northern extent of the site. Based on the preliminary road grades shown in the accompanying drawing, the road slopes range from approximately 0.5% to 3.2% within the overall site.

In accordance with the recommendations stated within the GHD Water Distribution Study (GHD, 2019), the maximum ground elevation within the site has been limited to 185.00m.

A noise berm has been proposed along the western limit of the site, due to the adjacent Gio Rail tracks. The berm has a varying peak elevation in accordance with the noise requirements and side slopes of approximately 2.5:1 on the western side and 3:1 on the eastern side.

CONCLUSIONS AND RECOMMENDATIONS

The following shall summarize the conclusions and recommendations found above:

Water Servicing

- The existing 400mm diameter cast iron watermain on the western limit of the site shall be rerouted within the proposed roadways with a new 400mm diameter PVC watermain. The proposed watermain will have connections at the Forks Road and Crescent Drive intersection and the north western limit of the site as shown in the enclosed Overall Watermain Distribution Plan. The portions of the cast iron watermain where flow has been rerouted shall be decommissioned and abandoned per discussions with the City of Welland.
- The site shall be limited to a maximum ground elevation of 185.00m to ensure a minimum water pressure of 40 psi is maintained within the entire site.
- Further analysis of the existing infrastructure will need to be undertaken as part of the design for the future John Deere development to ensure there is adequate capacity to accommodate the projected population.
- The site shall be serviced with watermain ranging from 150mm to 400mm in diameter.



Sanitary Servicing

- The gravity sanitary sewers on Forks Road, east of Crescent Drive shall be upgraded from 250mm to 375mm diameter sewers up to the entrance at Street A. The existing inverts and grade of the existing 250mm diameter sewer are adequate to convey the peak sanitary flows with the upgraded sanitary sewer size.
- The existing 450mm diameter trunk sanitary sewer on Crescent Drive has adequate capacity to convey sanitary flows from the proposed development to the Dain City Sewage Pumping Station.
- The site shall be serviced with sanitary sewers ranging from 200mm to 375mm in diameter.
- Following the upgrades to the Dain City pumping station, there will be adequate capacity within the existing infrastructure to service the site.
- Further analysis of the existing infrastructure will need to be undertaken as part of the design for the future John Deere development to ensure there is adequate capacity to accommodate the projected population.

Stormwater Management

- A stormwater management wet pond and dry detention facility are proposed to provide stormwater quality and quantity controls for the site prior to discharging to the Welland Canal. Per the requirements of the City of Welland and the MECP, quality controls shall be provided to an MECP Normal level (705 TSS Removal). Per the requirements of the SLSMC, quantity controls shall be provided up to the 100 year design storm event.
- Per the requirements of the City of Welland and the MECP, a Hydroworks HG4 oil/grit separator, or approved equivalent, has been proposed to provide stormwater quality controls to an MECP Normal level (70% TSS Removal) prior to discharging ultimately to the Old Welland Canal. Since the peak flows have been reduced as a result of the proposed development, stormwater quantity controls are not considered necessary for the storm sewers discharging ultimately to the Old Welland Canal.
- The site can be serviced by mainline storm sewers ranging from 300mm to 1650mm in diameter.

Preliminary Grading

• The site will be graded such that the majority of the site overland flows are conveyed within the roadways to the park lands located between Streets B and G, with road slopes ranging from approximately 0.5% approximately 3.2%.



• A maximum grade of 185.00m has been maintained within the site per the water servicing requirements.

Based on the above and the accompanying Servicing Plans, we are of the opinion that there exists adequate municipal servicing for this development. We trust the above comments are satisfactory for approval. If you have any questions or require additional information, please do not hesitate to contact our office.

Prepared By:

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Reviewed By:

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Encl.

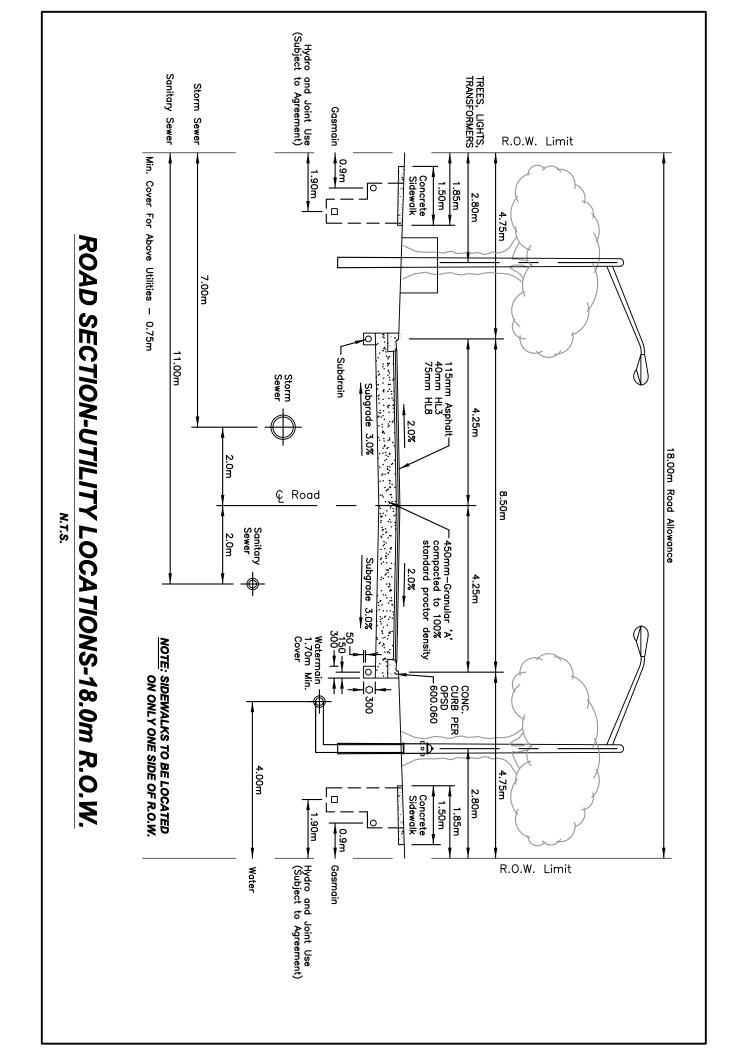


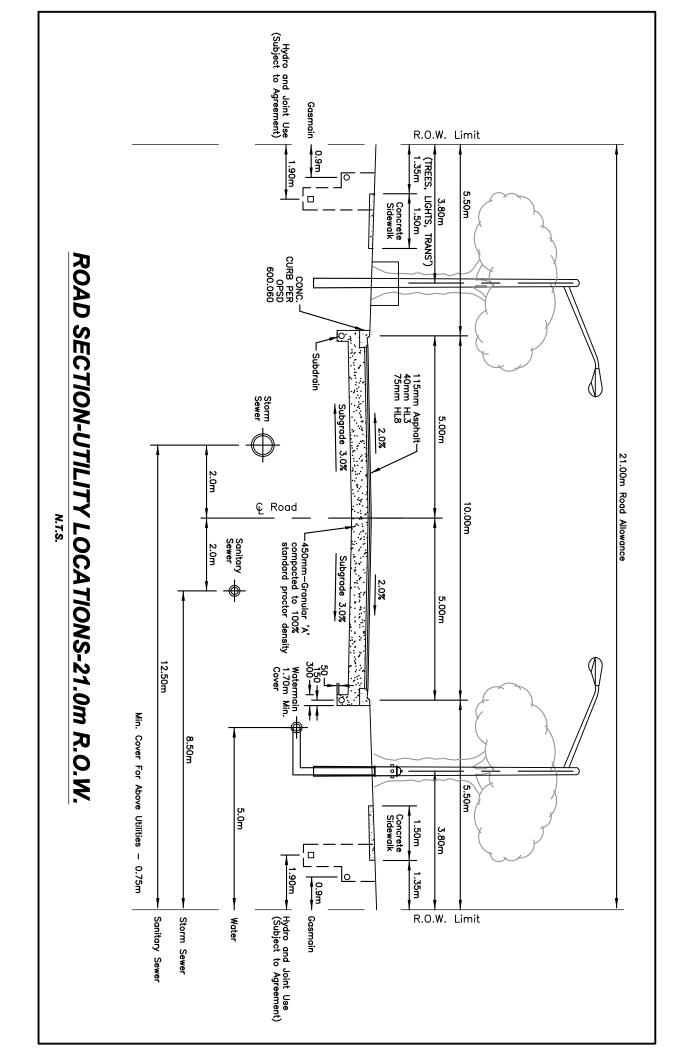
APPENDICES

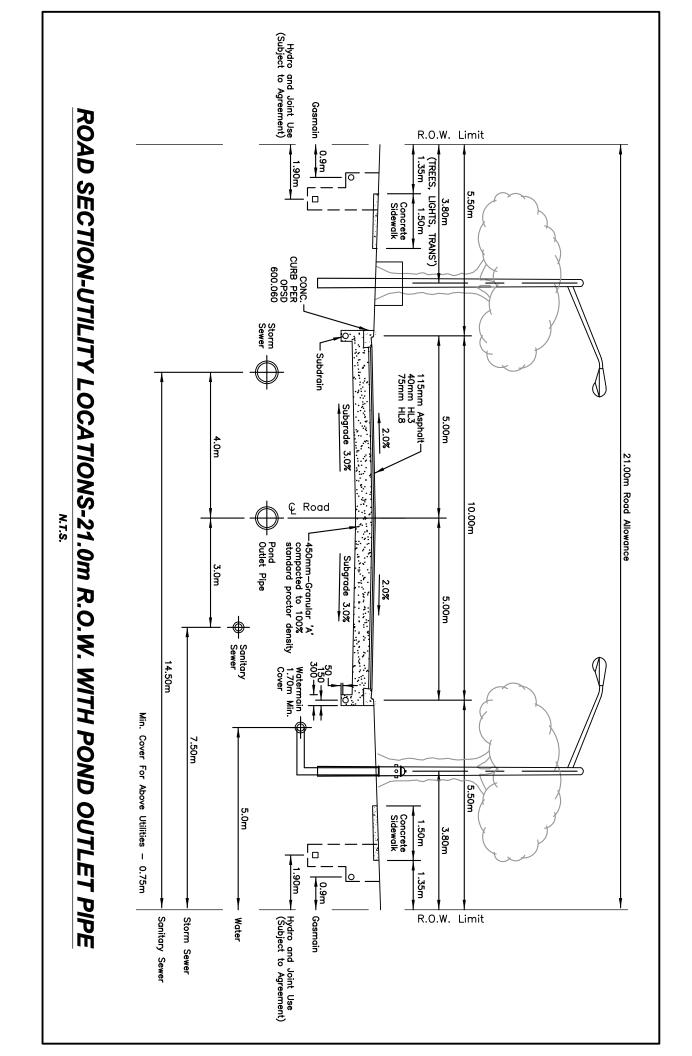


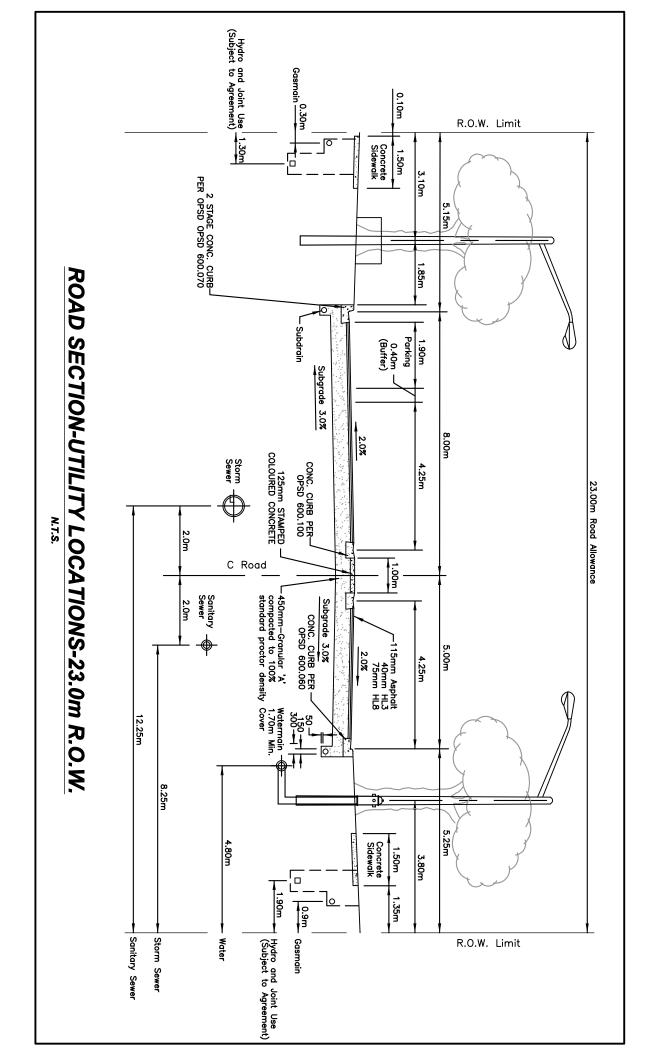
APPENDIX A

Proposed Typical 18m R.O.W. Cross Section Proposed Typical 21m R.O.W. Cross Section Proposed Typical 21m R.O.W. Cross Section w/ Storm Outlet Pipe Proposed Typical 23m R.O.W. Cross Section











APPENDIX B GHD Memorandum – Dated December 3, 2019





December 3, 2019

Subject:	Empire Homes Development – Water Distribut	tion System Reviev	v	
CC:				
From:	Samantha McCauley, P.Eng	Tel:	905-346-3857	
To:	Marvin Ingebrigsten, P.Eng	Ref. No.:	11155923	

1. Introduction

GHD was retained by the City of Welland to review the impacts of the proposed Empire Homes Development on the Welland water distribution system. Figure 1.1, attached at end, shows the location of the proposed development, which is broken up into three areas – Dain City Residential, Former John Deere, and Canal Bank/Dain Avenue.

Results of the completed analysis are described herein.

2. Model Set Up

2.1 Existing Model

The City of Welland's existing InfoWater all pipe water model was used as the base for the completion of this analysis. A model review was last conducted in 2018 with recent watermain construction projects incorporated, and updates made to the Welland Water Treatment Plant (WTP), including addition of pump curves for recently replaced pumps, and modification of base operational settings (on/off pump settings) to match settings determined from a review of 2017 SCADA data.

The City of Welland's existing InfoWater model also includes future development scenarios (average day and maximum day extended period simulations). These future development scenarios incorporate planned developments previously reviewed. These developments include:

- GE Plant (Built)
- Canal View Heights (Built/In construction)
- Hunter's Pointe Development Area (Future)
- Northern Reach Land Development (Future)
- Sauer Avenue, Louise Street, and Station Street (Future)

The review of the Empire Homes Development was completed using the future development scenarios.





2.2 Empire Homes Development Demands

Populations were provided by WSP for the proposed Empire Homes Development. Average day demands (ADD) were calculated using a per capita demand of 320 L/cap-day, a value which the City previously selected for use for development reviews. Maximum day demands (MDD) were calculated using a peaking factor of 1.5, which is the peaking factor used in the model established from historical demand data. The peak hour demand (PHD) peaking factor, which is based on the model MDD EPS demand pattern, is 1.87 (2.81 x ADD). Similar to the MDD peaking factor, the PHD peaking factor is based on historical demand data. Table 2.1 summarizes the demands assigned to the model for the Empire Homes Development, along with the resulting PHD.

Location	Population	ADD (L/s)	MDD (L/s)	PHD (L/s)
Former John Deere	3200	11.85	17.78	33.25
Dain City Residential	2990	11.07	16.61	31.06
Canal Bank/Dain Avenue	6983	25.86	38.79	72.54
Total	13173	48.78	73.18	136.85

Table 2.1 Empire Homes Development Demands

In addition to the demands noted above, a fire flow was also required to be used to assess the MDD + Fire Flow condition. The proposed development includes a mix of land uses, including single and multi-family units. The City's single family residential fire flow requirement is 67 L/s, while the City's requirement for multi-family units and some commercial properties is 133 L/s. A fire flow of 133 L/s was selected for the purpose of this analysis as it is a better representation of the fire flow needs for the development as a whole. This fire flow is applied at hour 7:00 of the MDD EPS scenario.

2.3 Development Servicing

Watermains and junctions were added to the model to represent the Empire Homes Development. Since a proposed servicing plan was not provided, watermain locations were assumed, with only watermains forming the assumed backbone of the servicing scheme (i.e. watermains connecting to the existing distribution network) included. Elevations were assigned to the junctions added to the model using the City's 1 m contours with the highest elevation for each area assigned. Figure 2.1 shows the watermains and junctions added to the model, including watermain sizing and assigned junction ground elevations. All pipes were assigned a C-Factor of 135, consistent with the C-Factor for plastic pipe established when the City's model was calibrated.

3. Review of Storage Requirements

Prior to completing the hydraulic analysis for the Empire Homes Development, a review of the City of Welland's overall storage capacity and existing and future storage requirements was completed. Per the MECP Design Guidelines for Drinking Water Systems, storage requirements for a water distribution system are as follows:

- Equalization Storage (A) = 25% of Maximum Day Demand
- Fire Storage (B) = 378 L/s for 6 hours (Based on MECP Equivalent Population Fire Flow Requirement)
- Emergency Storage (C) = 25% of A+B



The additional storage required for Empire Homes is 2.0 ML.

The total existing storage capacity was determined from the Region of Niagara Master Plan (2016). Table 3.1 summarizes the existing storage capacity, the existing and future storage requirement calculated in the master plan, and the existing and future storage requirement with and without the Empire Homes Development, calculated using the model demands and the procedure outlined above. As shown, the master plan appears to have included sufficient demand to account for the Empire Homes Development. Both the master plan and the model based calculations indicate that there is sufficient storage in the existing system to support the addition of the Empire Homes Development.

Table 3.1 Review of Storage Requirements

Description	Storage (ML)
Total Available Storage	37.0
Existing Required Storage – Master Plan	18.5
2041 Required Storage – Master Plan	21.6
Future Required Storage without Empire Homes Development – Model Demands	18.4
Future Required Storage with Empire Homes Development – Model Demands	20.4

4. Hydraulic Analysis

4.1 Design Criteria

In reviewing the impact of the Empire Homes Development on the existing distribution system, the following design criteria, as per City of Welland design standards and the MECP Design Guidelines for Drinking Water Systems, were used:

- Preferred system pressure between 350 to 550 kPa (50 to 80 psi)
- Minimum system pressure during normal operating conditions to be greater than 275 kPa (40 psi)
- Maximum system pressure during normal operating conditions to be less than 700 kPa (100 psi)
- System pressure with a 133 L/s fire flow during MDD to be greater than 140 kPa (20 psi)

4.2 Normal Operating Condition

Table 4.1 summarizes the minimum pressure during the ADD and MDD EPS scenarios within the proposed development with the existing water treatment plant pumping scheme.

Junction ID	Location	Junction Elevation	Minimum ADD EPS Pressure	Minimum MDD EPS Pressure
435701WJ01	Former John Deere	177 m	375 kPa (54 psi)	364 kPa (53 psi)
J-EH-1	Former John Deere	177 m	373 kPa (54 psi)	358 kPa (52 psi)
J-EH-2	Canal Bank/Dain Avenue	178 m	361 kPa (52 psi)	324 kPa (47 psi)
J-EH-3	Canal Bank/Dain Avenue	178 m	364 kPa (53 psi)	364 kPa (53 psi)
J-EH-4	Dain City Residential	189 m	257 kPa (37 psi)	243 kPa (35 psi)
J-EH-5	Canal Bank/Dain Avenue	177 m	373 kPa (54 psi)	347 kPa (50 psi)

Table 4.1 Empire Homes Development Normal Operating Pressures



As shown, pressures meet the design criteria at all locations with the exception of the Dain City Residential area, which does not meet the minimum 275 kPa (40 psi) requirement. The lower pressures in the Dain City Residential area are predominately due to the high ground elevation (maximum of 189 m) in this area in comparison to the hydraulic grade line of the system.

The top water level of the Bemis Elevated Tank, which represents the maximum hydraulic grade line of the system, is 219m – based on this top water level, and before accounting for any losses, the maximum pressure in the Dain City Residential area (at an elevation of 189 m) would, therefore, only be 294 kPa (43 psi). The low pressures in this area are further exacerbated by the current operating procedures at the WTP, where high lift pumps are shut down mid-morning, coinciding with periods of higher demand. Table 4.2 summarizes the minimum and maximum WTP flow and the minimum and maximum tank percent full with and without the Empire Homes Development. Note that both with and without the Empire Homes Development, the minimum percent full for the Bemis Tank coincides with the mid-morning WTP shutdown, while the maximum WTP flow coincides with the filling period that occurs when the WTP pumps turn back on after this mid-morning shutdown.

Parameter	Without Empire H	omes Development	With Empire Homes Development		
	Minimum	Maximum	Minimum	Maximum	
ADD EPS WTP Flow	0 L/s	326 L/s	0 L/s	328 L/s	
ADD EPS Bemis Tank % Full	77%	100%	65%	100%	
MDD EPS WTP Flow	0 L/s	789 L/s	0 L/s	799 L/s	
MDD EPS Bemis Tank % Full	72%	100%	63%	100%	

Table 4.2 Minimum and Maximum WTP Flow and Bemis Elevated Tank Volume

As shown in Table 4.2, with the addition of the Empire Homes development, there is an increase in the amount of drawdown that occurs at the Bemis Tank during the WTP mid-morning shutdown. The tank percent full of 63% that occurs during MDD EPS with the addition of the Empire Homes Development, corresponds to an HGL of 215.4 m, which is significantly lower than what it is needed to supply 275 kPa (40 psi) to the Dain City Residential area.

Modifying the WTP operating procedures, so that pumps are no longer off during mid-morning higher demand periods, would increase the minimum pressure in this area to above the MECP minimum; however, this strategy is not preferred since it relies exclusively on the operations of the WTP and limits the effective operating range of the Bemis Tank. Alternatively, limiting the ground elevation in the Dain City Residential area to 185 m would also increase the pressure to above 275 kPa (40 psi) without any modifications to the existing pumping scheme. Installation of a small booster pumping station to supply this area could also be considered as an alternative. Replacing the old cast iron watermain on Forks Road and increasing the size of the proposed watermain in this area was also reviewed as an alternative to limit headloss, however this would not increase the pressure to above 275 kPa (40 psi) due to the issue with the Bemis Tank HGL discussed above.

In addition to the pressures within the proposed Empire Homes Development, the pressures of the existing system were also reviewed. The addition of the Empire Homes Development results in a minor drop in pressure for the remainder of the system. The average drop to ADD pressure is 12 kPa (1.7 psi) and the average drop to MDD pressure is 17 kPa (2.5 psi). All system pressures in the existing network remain above 275 kPa (40 psi).



4.3 Fire Flow

Table 4.3 summarizes the available fire flow at each of the junctions added to the model to represent the Empire Homes Development. As shown, the existing system is capable of supplying greater than 133 L/s of fire flow (during MDD) to this development.

Junction ID	Location	Available Fire Flow during MDD (L/s)
435701WJ01	Former John Deere	248
J-EH-1	Former John Deere	174
J-EH-2	Canal Bank/Dain Avenue	173
J-EH-3	Canal Bank/Dain Avenue	191
J-EH-4	Dain City Residential	143
J-EH-5	Canal Bank/Dain Avenue	136

Table 4.3 Empire Homes Available Fire Flow

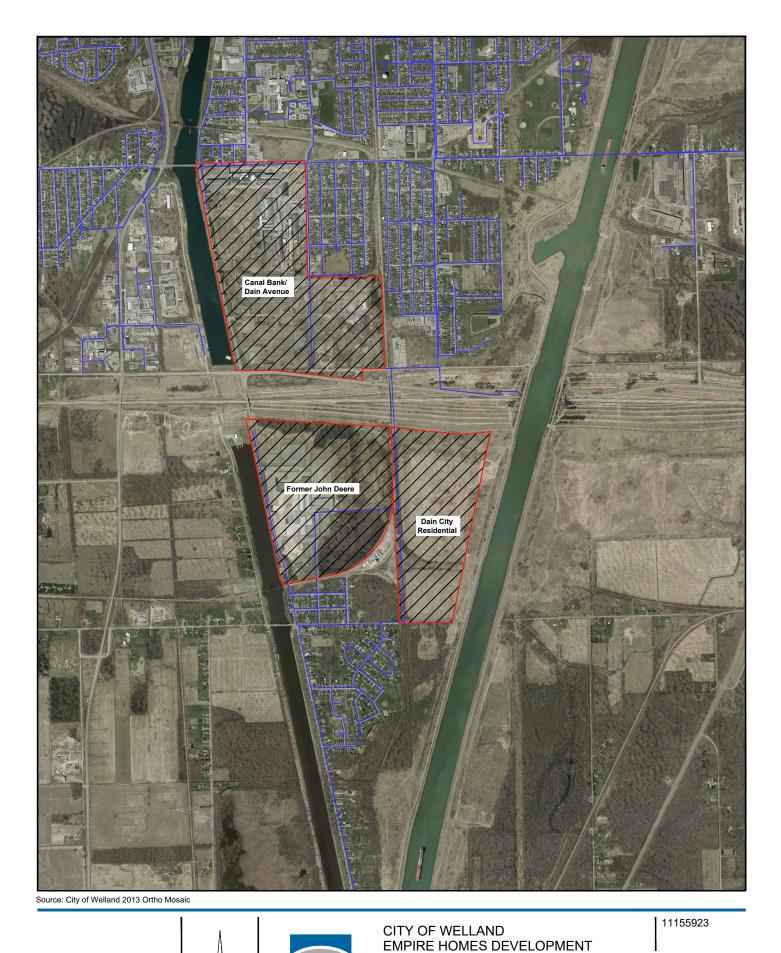
Additionally, the impact of the Empire Homes Development on the available fire flow within the existing system is minor, with many of the hydrants in the vicinity of the development having improved fire flow due to increased looping within the system. For hydrants within the existing system that do experience a drop in available fire flow with the addition of the Empire Homes Development, the average drop is approximately 1.3 L/s and does not change the NFPA 291 classification of the hydrant.

5. Conclusions and Recommendations

The City of Welland's water distribution system can supply water demand and fire flow to the proposed Empire Homes Development. This development will result in minor reductions in existing system pressure and available fire flow; however existing pressures will remain within MECP requirements.

During normal operating procedures, adequate pressure can be supplied to the Former John Deere and Canal Bank/Dain Avenue development areas without any modifications to the existing system operating procedures. However, the elevation in the Dain City Residential area (maximum elevation of 189m) results in pressures below the MECP recommendation of 275 kPa (40 psi) during high demand periods while the WTP is offline (mid-morning). Although these low pressures can be mitigated through changes to the operations of the WTP (eliminating mid-morning shut down), this strategy is not preferred since it relies exclusively on the operations of the WTP and limits the effective operating range of the Bemis Tank. Instead, the City should consider limiting the elevation of this portion of the development to a maximum of 185 m. Alternatively, a small booster station for this area could be considered.

Once a site servicing plan is developed, the Empire Homes Development should be reassessed to confirm required watermain sizing and connection locations to the existing system. Phasing plans should also be reviewed once available to confirm that suitable pressure and fire flow can be supplied not only during full buildout but during all interim phases.



LOCATION PLAN

GH

FIGURE 1.1

CAD File: I:\Project\Random Modelling\Empire Homes\Empire Homes Figure 1.1.dwg

NTS



Source: City of Welland 2013 Ortho Mosaic

NTS



WATER SERVICING

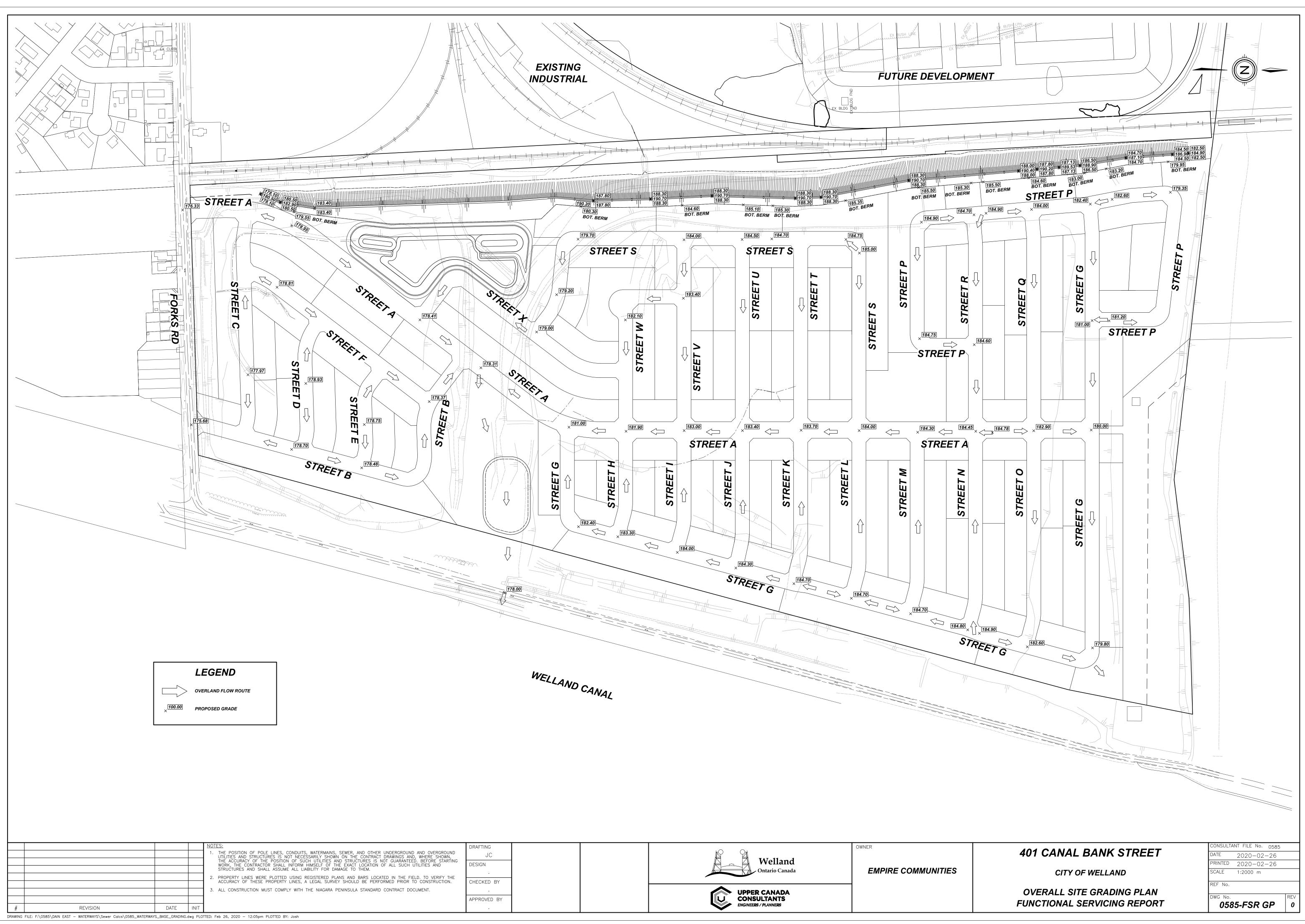
EMPIRE HOMES DEVELOPMENT

CITY OF WELLAND

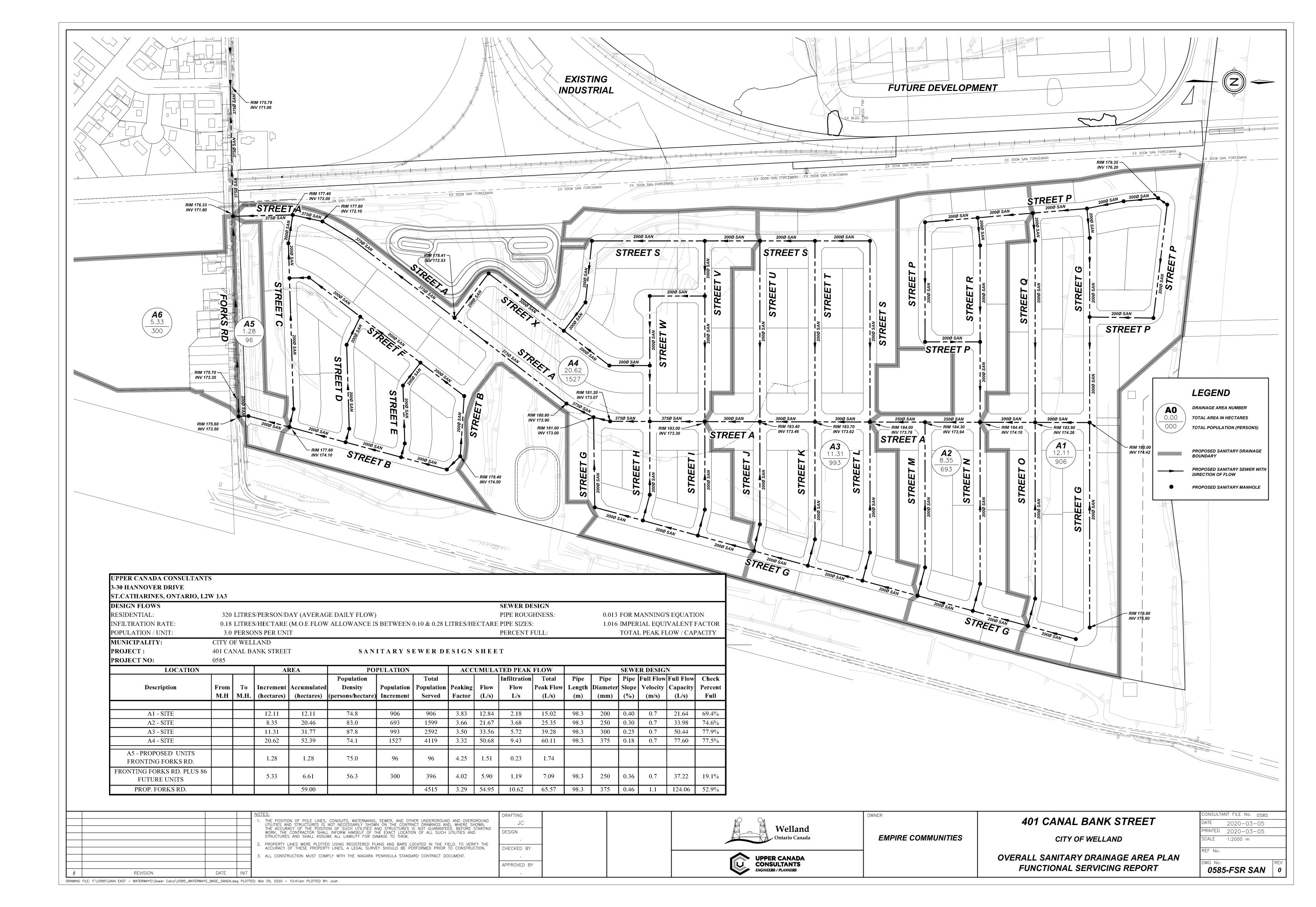
FIGURE 2.1

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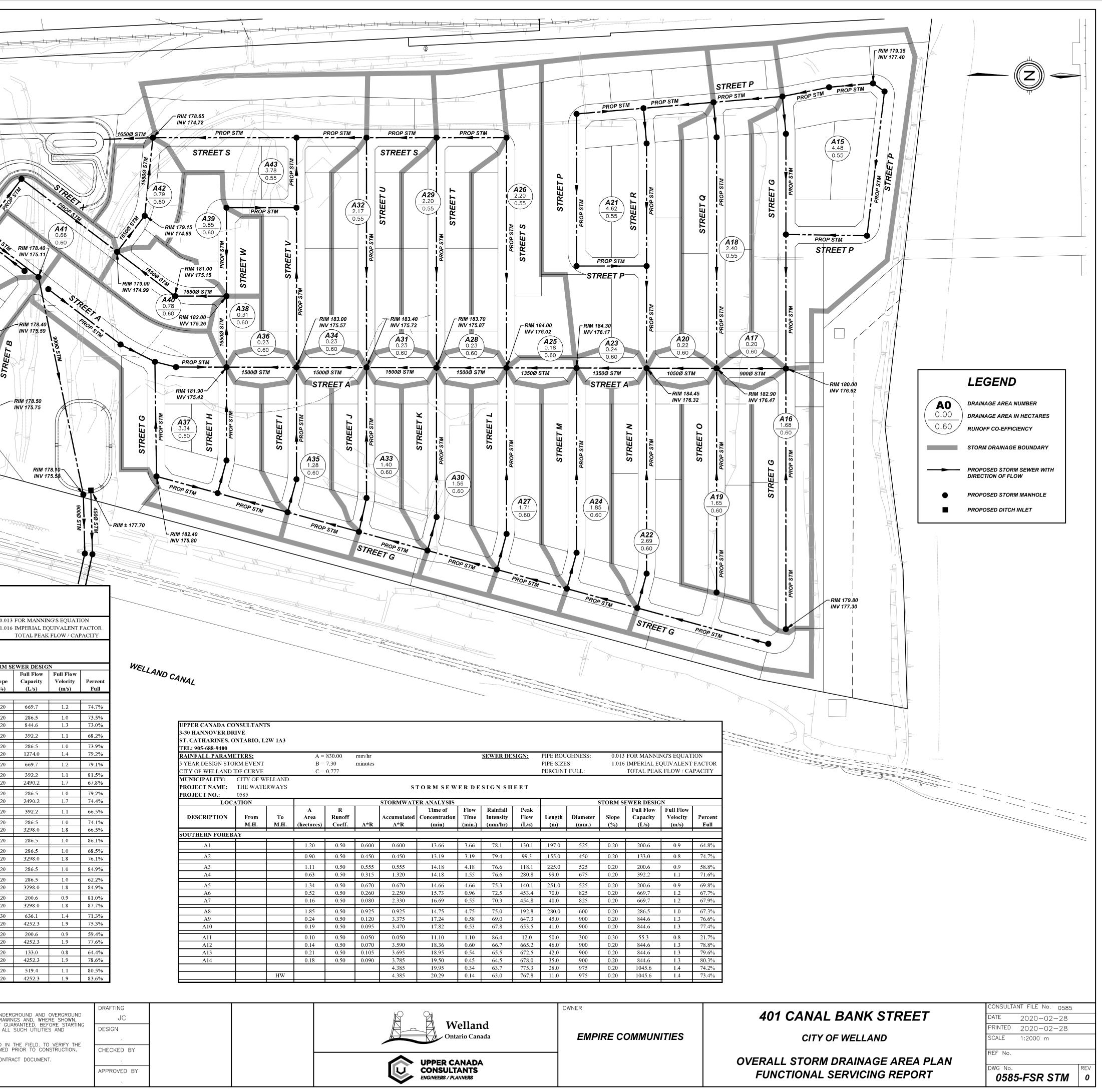
CAD File: I:\Project\Random Modelling\Empire Homes\Empire Homes Figure 2.1.dwg

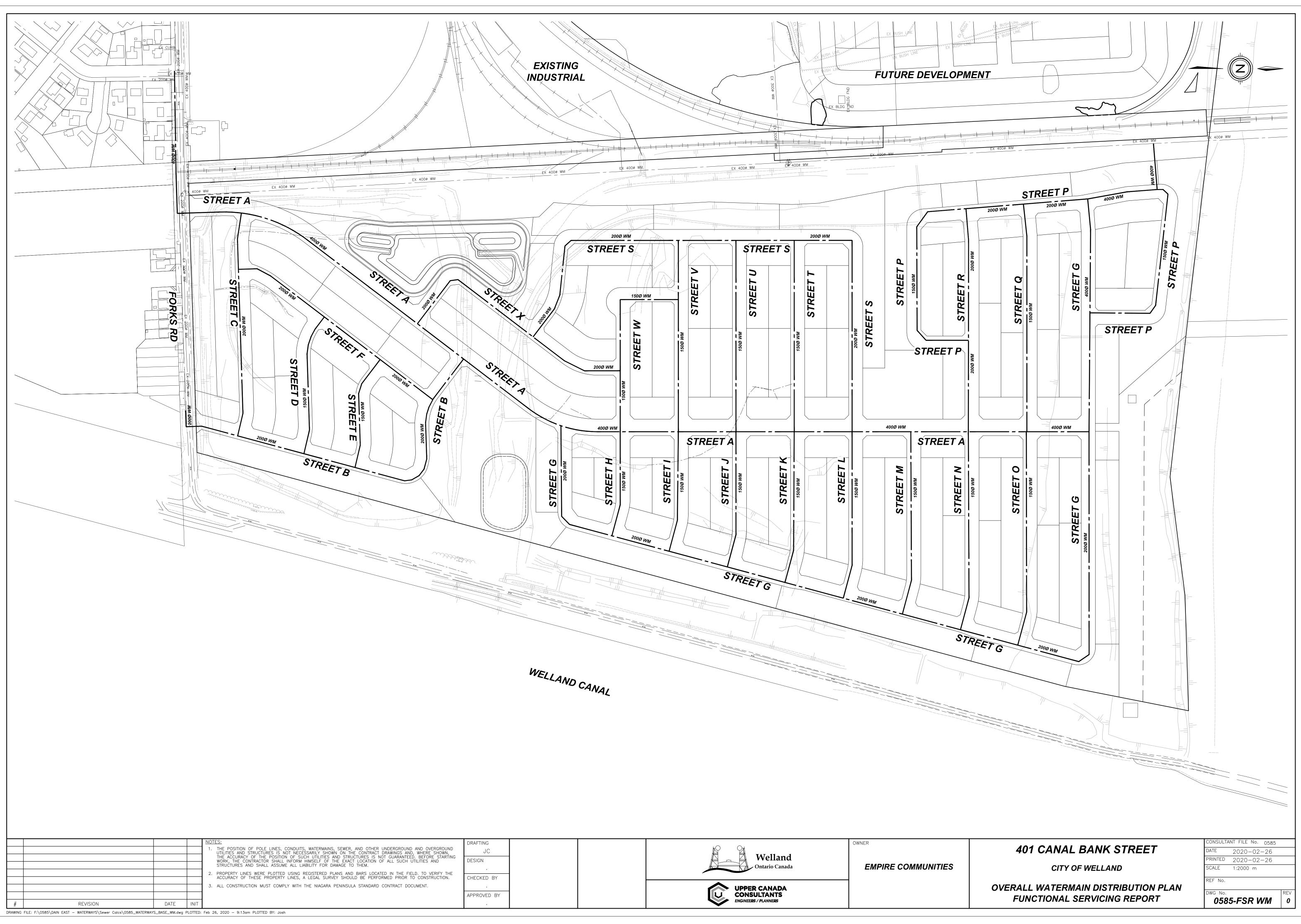


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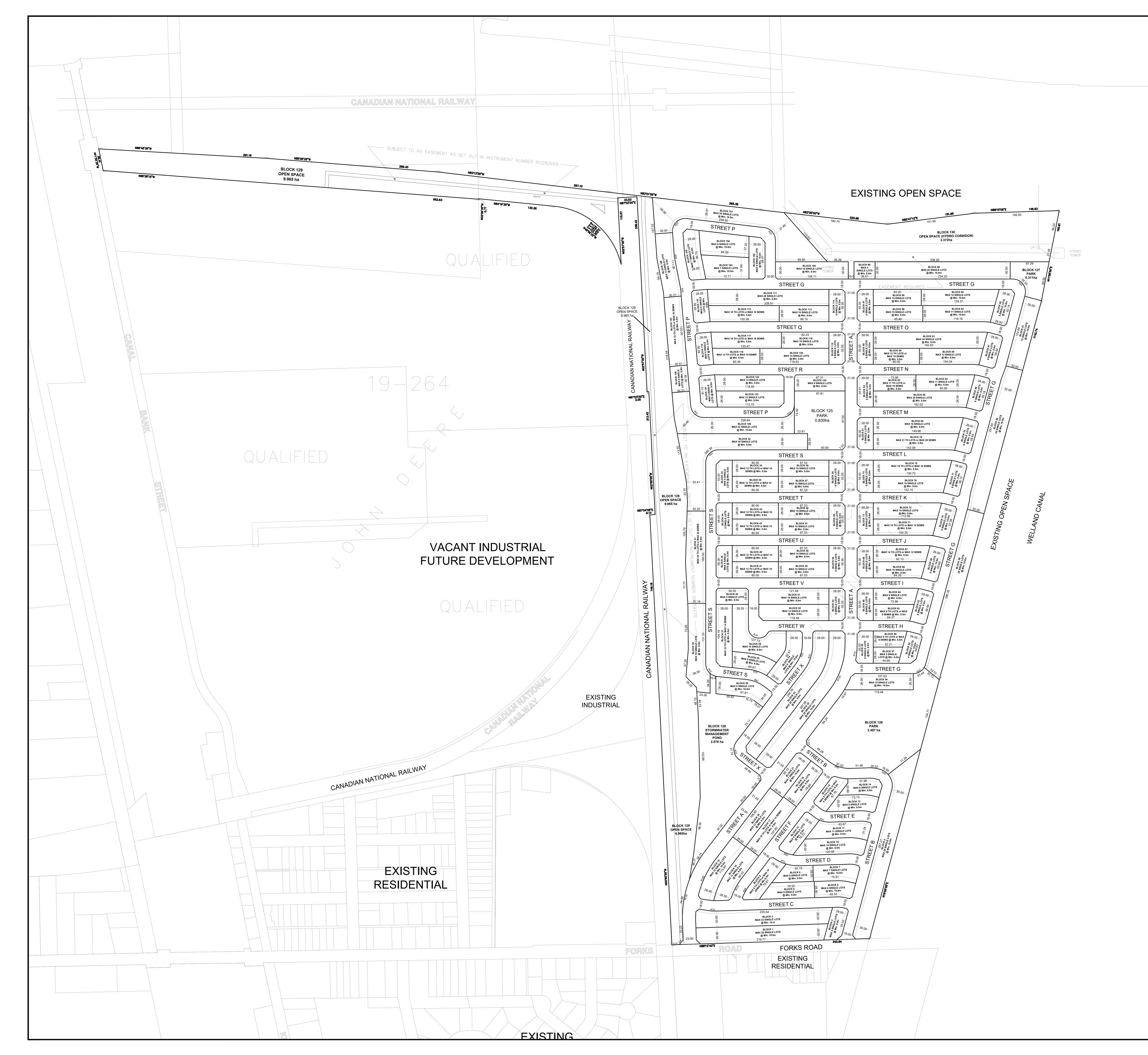


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A340.230.600.13818.38125.690.6854.92801.274.01500A351.280.600.7680.76814.324.3276.2162.5233.052554.0A360.230.600.13819.28726.370.2554.02892.927.01500A373.340.602.0042.00412.542.5481.4453.3213.0750A380.310.600.18621.47726.620.6553.73203.075.01650A390.850.600.5100.51011.731.7384.1119.293.0525A400.780.600.46822.45527.271.1352.93300.0131.01650A410.660.600.3960.39613.723.7277.985.7181.0450A420.790.600.47423.32528.401.1351.63343.0131.01650A433.780.552.0792.07915.785.7872.4418.2395.0750	3-30 HANNOVER D ST. CATHARINES, TEL: 905-688-9400 RAINFALL PARAM 5 YEAR DESIGN STO CITY OF WELLAND MUNICIPALITY: PROJECT NAME: PROJECT NO.: LOO DESCRIPTION NORTHERN FORE A15 A16 A17 A18 A19 A20 A21 A22 A23 A24 A22 A23 A24 A25 A26 A27 A28 A29 A30	ORIVE ONTARIO, L2 ORM EVENT DIDF CUR VE CITY OF W THE WATE 0585 CATION From M.H.	2W 1A3 ELLAND RWAYS To	B = C = C = A Area (hectares) 4.48 1.68 0.20 2.40 2.40 2.40 1.65 0.22 4.62 2.69 0.24 1.85 0.18 2.20 1.71 0.23 2.20 1.56	= 7.30 = 0.777 Runoff Coeff. 0.55 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.55 0.60 0.55 0.60 0.55 0.60	minutes A*R 2.464 1.008 0.120 1.320 0.990 0.132 2.541 1.614 0.144 1.110 0.108 1.210 1.026 0.138 1.210 0.936	STORMWAT Accumulated A*R 2.464 1.008 3.592 1.320 0.990 6.034 2.541 1.614 10.333 1.110 11.551 1.210 1.026 13.925 1.210 0.936	TER ANALYSIS Time of Concentration (min) 15.49 14.69 20.99 15.57 14.02 22.00 14.75 16.25 22.86 15.30 23.59 13.81 14.94 24.33 15.38 14.60	Flow Time (min.) 5.49 4.69 1.01 5.57 4.02 0.87 4.75 6.25 0.73 5.30 0.73 5.30 0.73 3.81 4.94 0.68 5.38 4.60	E SIGN SH Rainfall Intensity (mm/hr) 73.1 75.2 61.8 72.9 77.0 60.2 75.0 71.3 58.8 73.6 57.7 71.6 74.5 56.7 73.4 75.4	E E T Peak Flow (L/s) 500.5 210.6 616.9 267.4 211.8 1008.5 529.6 319.6 1688.3 227.0 1852.5 260.8 212.4 2193.0 246.7 196.1	PIPE SIZI PERCENT Length (m) 400.0 276.0 78.0 237.0 74.0 3355.0 237.0 74.0 346.0 398.0 74.0 312.0 74.0 243.0 291.0 74.0 317.0 291.0	ES: T FULL: Diameter (mm.) 825 600 900 675 600 1050 825 675 1350 600 1350 600 1350 600 1500 600 1500 600	
A360.230.600.13819.28726.370.2554.02892.927.01500A373.340.602.0042.00412.542.5481.4453.3213.0750A380.310.600.18621.47726.620.6553.73203.075.01650A390.850.600.5100.51011.731.7384.1119.293.0525A400.780.660.46822.45527.271.1352.9330.0131.01650A410.660.600.3960.39613.723.7277.985.7181.0450A420.790.600.47423.32528.401.1351.63343.0131.01650A433.780.552.0792.07915.785.7872.4418.2395.0750	3-30 HANNOVER D ST. CATHARINES, TEL: 905-688-9400 RAINFALL PARAM 5 YEAR DESIGN STO CITY OF WELLAND MUNICIPALITY: PROJECT NAME: PROJECT NO.: LOO DESCRIPTION NORTHERN FORE A15 A16 A17 A18 A19 A20 A21 A22 A22 A23 A24 A25 A24 A25 A26 A27 A28 A29 A30 A31 A32	ORIVE ONTARIO, L2 ORM EVENT DIDF CUR VE CITY OF W THE WATE 0585 CATION From M.H.	2W 1A3 ELLAND RWAYS To	B = C	= 7.30 = 0.777 Runoff Coeff. 0.55 0.60 0.55 0.60 0.55	minutes A*R 2.464 1.008 0.120 1.320 0.990 0.132 2.541 1.614 0.144 1.110 0.108 1.210 1.026 0.138 1.210 0.936 0.138 1.194	STORMWAT Accumula ted A*R 2.464 1.008 3.592 1.320 0.990 6.034 2.541 1.614 10.333 1.110 11.551 1.210 1.026 13.925 1.210 0.936 16.209 1.194	TER ANALYSIS Time of Concentration (min) 15.49 14.69 20.99 15.57 14.02 22.00 14.75 16.25 22.86 15.30 23.59 13.81 14.94 24.33 15.38 14.60 25.01 15.38	Flow Time (min.) 5.49 4.69 1.01 5.57 4.02 0.87 4.75 6.25 0.73 5.30 0.73 5.30 0.73 3.81 4.94 0.68 5.38 4.60 0.68 5.38	E SIGN SH Rainfall Intensity (mm/hr) 73.1 75.2 61.8 72.9 77.0 60.2 75.0 71.3 58.8 73.6 57.7 71.6 74.5 56.7 73.4 75.4 55.8 73.4	E E T Peak Flow (L/s) 500.5 210.6 616.9 267.4 211.8 1008.5 529.6 319.6 1688.3 227.0 1852.5 260.8 212.4 219.3 246.7 196.1 2510.7 243.3	PIPE SIZI PERCENT Length (m) 400.0 276.0 78.0 237.0 74.0 3355.0 237.0 74.0 346.0 398.0 74.0 312.0 74.0 243.0 291.0 74.0 317.0 271.0 74.0 317.0	ES: T FULL: Diameter (mm.) 825 600 900 675 600 1050 825 675 1350 600 1350 600 1350 600 1350 600 1500 600 1500 600	
A380.310.600.18621.47726.620.6553.73203.075.01650A390.850.600.5100.51011.731.7384.1119.293.0525A400.780.600.46822.45527.271.1352.93300.0131.01650A410.660.600.3960.39613.723.7277.985.7181.0450A420.790.600.47423.32528.401.1351.63343.0131.01650A433.780.552.0792.07915.785.7872.4418.2395.0750	3-30 HANNOVER D ST. CATHARINES, TEL: 905-688-9400 RAINFALL PARAM 5 YEAR DESIGN STO CITY OF WELLAND MUNICIPALITY: PROJECT NAME: PROJECT NO.: LOO DESCRIPTION NORTHERN FORE A15 A16 A17 A18 A19 A20 A21 A22 A23 A24 A25 A26 A27 A30 A31 A32 A33	ORIVE ONTARIO, L2 ORM EVENT DIDF CUR VE CITY OF W THE WATE 0585 CATION From M.H.	2W 1A3 ELLAND RWAYS To	B = C	= 7.30 = 0.777 Runoff Coeff. 0.55 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.55 0.60 0.55 0.60 0.55 0.60 0.55 0.60 0.55 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60	minutes A*R 2.464 1.008 0.120 1.320 0.990 0.132 2.541 1.614 0.144 1.110 0.108 1.210 1.026 0.138 1.210 1.026 0.138 1.210 0.936 0.138 0.9 0.138 0.9 0.138 0.9 0.138 0.9 0.138 0.9 0.138 0.9 0.138 0.9 0.138 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	STORMWAT Accumula ted A*R 2.464 1.008 3.592 1.320 0.990 6.034 2.541 1.614 10.333 1.110 11.551 1.210 1.026 13.925 1.210 0.936 16.209 1.194 0.840 18.381	TER ANALYSIS Time of Concentration (min) 15.49 14.69 20.99 15.57 14.02 22.00 14.75 16.25 22.86 15.30 23.59 13.81 14.94 24.33 15.38 14.60 25.01 15.38 14.25 25.69	Flow Time (min.) 5.49 4.69 1.01 5.57 4.02 0.87 4.75 6.25 0.73 5.30 0.73 5.30 0.73 3.81 4.94 0.68 5.38 4.60 0.68 5.38	E SIGN SH Rainfall Intensity (mm/hr) 73.1 75.2 61.8 72.9 77.0 60.2 75.0 71.3 58.8 73.6 57.7 71.6 74.5 56.7 73.4 75.4 55.8 73.4 75.4 55.8 73.4 75.4 54.9	E E T Peak Flow (L/s) 500.5 210.6 616.9 267.4 211.8 1008.5 529.6 319.6 1688.3 227.0 1852.5 260.8 212.4 2193.0 246.7 196.1 2510.7 243.3 178.3 2801.2	PIPE SIZI PERCEN Length (m) 400.0 276.0 78.0 355.0 237.0 74.0 346.0 398.0 74.0 312.0 74.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 74.0 317.0 250.0 74.0	ES: T FULL: Diameter (mm.) 825 600 900 675 600 1050 825 675 1350 600 1350 600 1350 600 1350 600 1350 600 1500 600 1500	
A40 0.78 0.60 0.468 22.455 27.27 1.13 52.9 3300.0 131.0 1650 A41 0.66 0.60 0.396 0.396 13.72 3.72 77.9 85.7 181.0 450 A42 0.79 0.60 0.474 23.325 28.40 1.13 51.6 3343.0 131.0 1650 A43 3.78 0.55 2.079 2.079 15.78 5.78 72.4 418.2 395.0 750	3-30 HANNOVER D ST. CATHARINES, TEL: 905-688-9400 RAINFALL PARAM 5 YEAR DESIGN STO CITY OF WELLAND MUNICIPALITY: PROJECT NAME: PROJECT NO.: LOO DESCRIPTION NORTHERN FORE! A15 A16 A17 A18 A19 A20 A21 A22 A23 A24 A22 A23 A24 A25 A26 A27 A26 A27 A28 A29 A30 A31 A32 A33 A34 A35 A36	ORIVE ONTARIO, L2 ORM EVENT DIDF CUR VE CITY OF W THE WATE 0585 CATION From M.H.	2W 1A3 ELLAND RWAYS To	B = C	= 7.30 = 0.777 Runoff Coeff. 0.55 0.60	minutes A*R 2.464 1.008 0.120 1.320 0.990 0.132 2.541 1.614 0.144 1.110 0.108 1.210 1.026 0.138 1.210 0.936 0.138 1.194 0.840 0.138 0.768 0.138 0.768 0.138 0.14	STORMWAT Accumulated A*R 2.464 1.008 3.592 1.320 0.990 6.034 2.541 1.614 10.333 1.110 11.551 1.210 1.026 13.925 1.210 0.936 16.209 1.194 0.840 18.381 0.768 19.287	Time of Concentration (min) 15.49 14.69 20.99 15.57 14.02 22.00 14.75 16.25 22.86 15.30 23.59 13.81 14.94 24.33 15.38 14.60 25.01 15.38 14.25 25.69 14.32 26.37	Flow Time (min.) 5.49 4.69 1.01 5.57 4.02 0.87 4.75 6.25 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.38 4.60 0.68 5.38 4.60 0.68 5.38 4.25 0.68 4.32 0.25	E SIGN SH Rainfall Intensity (mm/hr) 73.1 75.2 61.8 72.9 77.0 60.2 75.0 71.3 58.8 73.6 57.7 71.3 58.8 73.6 57.7 71.6 74.5 56.7 73.4 75.4 55.8 73.4 75.4 55.8 73.4 76.4 54.9 76.2 54.0	E E T Peak Flow (L/s) 500.5 210.6 616.9 267.4 211.8 1008.5 529.6 319.6 1688.3 227.0 1852.5 260.8 212.4 2193.0 246.7 196.1 2510.7 243.3 178.3 2801.2 162.5 2892.9	PIPE SIZI PERCEN Length (m) 400.0 276.0 78.0 237.0 74.0 3355.0 237.0 74.0 398.0 74.0 398.0 74.0 398.0 74.0 243.0 291.0 74.0 243.0 291.0 74.0 291.0 74.0 271.0 74.0 201.0 74.0	ES: T FULL: Diameter (mm.) 825 600 900 675 600 1050 825 675 1350 600 1050 825 675 1350 600 1350 600 1500 600 1500 600 1500 600 1500 600 1500	
A42 0.79 0.60 0.474 23.325 28.40 1.13 51.6 3343.0 131.0 1650 A43 3.78 0.55 2.079 2.079 15.78 5.78 72.4 418.2 395.0 750	3-30 HANNOVER D ST. CATHARINES, TEL: 905-688-9400 RAINFALL PARAM 5 YEAR DESIGN STOCHTY OF WELLAND MUNICIPALITY: PROJECT NAME: PROJECT NO.: LOO DESCRIPTION NORTHERN FORE A15 A16 A17 A18 A19 A20 A21 A22 A23 A24 A25 A26 A27 A30 A31 A32 A33 A34	ORIVE ONTARIO, L2 ORM EVENT DIDF CUR VE CITY OF W THE WATE 0585 CATION From M.H.	2W 1A3 ELLAND RWAYS To	B = C	7.30 = 0.777 Runoff Coeff. 0.55 0.60	minutes A*R 2.464 1.008 0.120 1.320 0.990 0.132 2.541 1.614 0.144 1.110 0.108 1.210 1.026 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.194 0.840 0.138 0.768 0.138	STORMWAT Accumula ted A*R 2.464 1.008 3.592 1.320 0.990 6.034 2.541 1.614 10.333 1.110 11.551 1.210 1.026 13.925 1.210 0.936 16.209 1.194 0.840 18.381 0.768 19.287 2.004 21.477	Time of Concentration (min) 15.49 14.69 20.99 15.57 14.02 22.00 14.75 16.25 22.86 15.30 23.59 13.81 14.94 24.33 15.38 14.60 25.01 15.38 14.25 25.69 14.32 26.37 12.54 26.62	Flow Time (min.) 5.49 4.69 1.01 5.57 4.02 0.87 4.75 6.25 0.73 5.30 0.73 5.30 0.73 5.30 0.73 3.81 4.94 0.68 5.38 4.60 0.68 5.38 4.60 0.68 5.38 4.25 0.68 4.32 0.25 2.54 0.65	E SIGN SH Rainfall Intensity (mm/hr) 73.1 75.2 61.8 72.9 77.0 60.2 75.0 71.3 58.8 73.6 57.7 77.6 74.5 56.7 74.5 56.7 73.4 75.4 55.8 73.4 75.4 55.8 73.4 75.4 55.8 73.4 75.4 55.8 73.4 76.4 54.9 76.2 54.0 81.4 53.7	E E T Peak Flow (L/s) 500.5 210.6 616.9 267.4 211.8 1008.5 529.6 319.6 1688.3 227.0 1852.5 260.8 212.4 2193.0 246.7 196.1 2510.7 243.3 178.3 2801.2 162.5 2892.9 453.3 3203.0	PIPE SIZI PERCEN Length (m) 400.0 276.0 78.0 237.0 74.0 3355.0 237.0 74.0 346.0 398.0 74.0 312.0 74.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 271.0 74.0 317.0 250.0 74.0 213.0 275.0	ES: T FULL: Diameter (mm.) 825 600 900 675 675 675 675 1350 600 1050 825 675 1350 600 1350 600 1350 600 1350 600 1500 600 1500 600 1500 600 1500 600 1500 600 1500 600 1500	
	3-30 HANNOVER D ST. CATHARINES, TEL: 905-688-9400 RAINFALL PARAM 5 YEAR DESIGN STOCITY OF WELLAND MUNICIPALITY: PROJECT NAME: PROJECT NO.: LOO DESCRIPTION NORTHERN FORE A15 A16 A17 A18 A19 A20 A21 A22 A23 A24 A25 A26 A27 A30 A31 A32 A33 A34 A35 A36	ORIVE ONTARIO, L2 ORM EVENT DIDF CUR VE CITY OF W THE WATE 0585 CATION From M.H.	2W 1A3 ELLAND RWAYS To	B = C	= 7.30 = 0.777 Runoff Coeff. 0.55 0.60	minutes A*R 2.464 1.008 0.120 1.320 0.990 0.132 2.541 1.614 0.144 1.110 0.120 1.210 1.210 0.936 0.138 1.210 0.936 0.138 1.194 0.840 0.138 0.768 0.138 2.004 0.510 0.510	STORMWAT Accumula ted A*R 2.464 1.008 3.592 1.320 0.990 6.034 2.541 1.614 10.333 1.110 11.551 1.210 1.026 13.925 1.210 0.936 16.209 1.194 0.840 18.381 0.768 19.287 2.004 21.477 0.510 22.455	Time of Concentration (min) 15.49 14.69 20.99 15.57 14.02 22.00 14.75 16.25 22.86 15.30 23.59 13.81 14.94 24.33 15.38 14.25 25.01 15.38 14.25 25.69 14.32 26.37 12.54 26.62 11.73 27.27	Flow Time (min.) 5.49 4.69 1.01 5.57 4.02 0.87 4.75 6.25 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.38 4.94 0.68 5.38 4.25 0.68 4.25 0.68 4.32 0.25 2.54 0.65 1.73 1.13	E SIGN SH Rainfall Intensity (mm/hr) 73.1 75.2 61.8 72.9 77.0 60.2 75.0 71.3 58.8 73.6 57.7 71.3 58.8 73.6 57.7 71.3 58.8 73.6 57.7 71.3 58.8 73.6 57.7 71.3 58.8 73.6 57.7 71.4 55.8 73.4 75.4 55.8 73.4 75.4 55.8 73.4 76.4 54.9 76.2 54.0 81.4 53.7 84.1 52.9	E E T Peak Flow (L/s) 500.5 210.6 616.9 267.4 211.8 1008.5 529.6 319.6 1688.3 227.0 1852.5 260.8 212.4 2193.0 246.7 196.1 2510.7 243.3 178.3 2801.2 162.5 2892.9 453.3 3203.0 119.2 3300.0	PIPE SIZI PERCEN Length (m) 400.0 276.0 78.0 355.0 237.0 74.0 346.0 398.0 74.0 312.0 74.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 74.0 317.0 250.0 74.0 250.0 74.0 250.0 74.0 250.0 74.0 250.0 74.0 213.0 75.0 93.0 131.0	ES: T FULL: Diameter (mm.) 825 600 900 675 600 1050 825 675 1350 600 1350 600 1350 600 1350 600 1500 600 1500 600 1500 600 1500 600 1500 525 1500	
	3-30 HANNOVER D ST. CATHARINES, TEL: 905-688-9400 RAINFALL PARAM 5 YEAR DESIGN STOCITY OF WELLAND MUNICIPALITY: PROJECT NAME: PROJECT NO.: LOO DESCRIPTION NORTHERN FORE A15 A16 A17 A18 A19 A20 A21 A22 A23 A24 A25 A26 A27 A30 A31 A32 A34 A35 A36	ORIVE ONTARIO, L2 ORM EVENT DIDF CUR VE CITY OF W THE WATE 0585 CATION From M.H.	2W 1A3 ELLAND RWAYS To	B = C	7.30 0.777 Runoff Coeff. 0.55 0.60	minutes A*R 2.464 1.008 0.120 1.320 0.990 0.132 2.541 1.614 0.144 1.110 0.108 1.210 1.026 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 1.210 0.936 0.138 0.	STORMWAT Accumula ted A*R 2.464 1.008 3.592 1.320 0.990 6.034 2.541 1.614 10.333 1.110 11.551 1.210 1.026 13.925 1.210 1.026 13.925 1.210 0.936 16.209 1.194 0.840 18.381 0.768 19.287 2.004 21.477 0.510 22.455 0.396	Time of Concentration (min) 15.49 14.69 20.99 15.57 14.02 22.00 14.75 16.25 22.86 15.30 23.59 13.81 14.94 24.33 15.38 14.25 25.01 15.38 14.25 25.69 14.32 26.37 12.54 26.62 11.73 27.27 13.72	Flow Time (min.) 5.49 4.69 1.01 5.57 4.02 0.87 4.75 6.25 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.30 0.73 5.38 4.94 0.68 5.38 4.60 0.68 5.38 4.25 0.68 4.32 0.25 2.54 0.65 1.73 1.13 3.72	E SIGN SH Rainfall Intensity (mm/hr) 73.1 75.2 61.8 72.9 77.0 60.2 75.0 71.3 58.8 73.6 57.7 71.3 58.8 73.6 57.7 77.6 74.5 56.7 73.4 75.4 55.8 73.4 75.4 55.8 73.4 75.4 55.8 73.4 75.4 55.8 73.4 75.4 55.8 73.4 76.4 54.9 76.2 54.0 81.4 53.7 84.1 52.9 77.9	E E T Peak Flow (L/s) 500.5 210.6 616.9 267.4 211.8 1008.5 529.6 319.6 1688.3 227.0 1852.5 260.8 212.4 2193.0 246.7 196.1 2510.7 243.3 178.3 2801.2 162.5 2892.9 453.3 3203.0 119.2 3300.0 85.7	PIPE SIZI PERCEN Length (m) 400.0 276.0 78.0 237.0 74.0 3355.0 237.0 74.0 3355.0 237.0 74.0 312.0 74.0 312.0 74.0 243.0 291.0 74.0 243.0 291.0 74.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 243.0 74.0 317.0 243.0 243.0 74.0 317.0 243.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 317.0 250.0 74.0 74.0 317.0 250.0 74.0 317.0 74.0 74.0 74.0 317.0 74.0 74.0 74.0 74.0 74.0 74.0 74.0 7	ES: T FULL: Diameter (mm.) 825 600 900 675 600 1050 825 675 1350 600 1350 600 1350 600 1350 600 1350 600 1350 600 1500 600 1500 600 1500 600 1500 525 1500 750 1650 750 1650	





	DRAFTING			OWNER
DERGROUND AND OVERGROUND AWINGS AND, WHERE SHOWN,	JC			
GUARANTEED. BEFORE STARTING ALL SUCH UTILITIES AND	DESIGN		Welland	
IN THE FIELD. TO VERIFY THE			Ontario Canada	EMPI
ED PRIOR TO CONSTRUCTION.	CHECKED BY			
NTRACT DOCUMENT.			UPPER CANADA	
	APPROVED BY		U CONSULTANTS	
			ENGINEERS / PLANNERS	



191.5111						Townline	5 Tunnel Rd	
KEY PI				N.T.S.	i			
	DNAL INFORMA der Section 51(17) ning Act R.S.O. 1990 c.)N					
b. SHOWN ON c. SHOWN ON d. LAND TO BE WITH LAND e. SHOWN ON	E USED IN ACCORDANCE USE SCHEDULE		g. h. j. k. l.	SHOWN ON DR MUNICIPAL PIPI SOIL IS SILTY SHOWN ON DR ALL MUNICIPAL SHOWN ON DR	ED WATE CLAY AFT PLA . SERVICI	R TO BE N ES TO BE	PRÓVIDED	
	DULE OF LAND ITE AREA - 72.1							
Proposed L		Unit		Reference Blocks 1-2,4	5719		Area (Ha.)	
<u>Residential</u>	Singles 10.0m	360)	Blocks 1 2,4 21,22,24, 29, 60,69,92-94,9 109 Blocks 3,6,8, 20,23,25,26,2 36-41,44,45,4 61,62,64-66,6 76-78,80-82,	54,58,5 98,101- ,10-14, 28,30,32 48-53,5 68,70,7	59, -105, 16,18, 2,33, 55,57, 2-74,	12.015	
	Singles 8.0m Townhomes 5.5m	725	5	95-97,99,100 110-111,113 <u>120-124</u> Blocks 9,15 35,42,43,46,4 71,75,79,83,8 117,119, Blocks 125-),106,1(-16,118 ,17,27,5 17,56,65 39,107,)8, 3, 31,34, 3,67,	18.864 6.273 3.639	
Open Space ROADS 21m - 23m	h R.O.W. (Street A) W. (Streets B-X)			Block 128 Blocks 129-	130		2.078 13.338 2.665 13.260	
TOTAL		140	5				72.132	
	Propose	d Su	mn	nary Yiel	d			
Residentia Residentia	oosed Unit Mix <u>1 Singles 10.0m</u> 1 Singles 8.0m 1 Townhomes 5.5r		A1	it Count ternate 5. Townhous Units 360 725 320	50m	with { Semi	it Count Alternate 5.50m -Detached Units 360 725	
	l Semi-Detached 5			1405			284 1 369	
5								
4								
3								
1 No.	REVIS	SION				DA	ATE	
REVIS								
WE, BEING T	R'S CERTIFI	OF TH	IE SL	JBJECT LAND				
DRAFT PLAN SIGNED	OF SUBDIVISION FOR A	\PPRO\	/AL.		DATE			
SURVEYOR'S CERTIFICATE I HEREBY CERTIFY THAT THE BOUNDARIES OF THE SUBJECT LANDS AND THEIR RELATIONSHIP TO THE ADJACENT LANDS ARE ACCURATELY AND CORRECTLY SHOWN ON THIS PLAN.								
SIGNED DATE FEBRUARY 20, 2020								
	I CITY EA FT PLAN				DI	VIS	SION	
PART LOTS 20, 21, 22 AND 23, CONCESSION 5, PART OF THE ROAD ALLOWANCE BETWEEN LOTS 20 AND 21, CONCESSION 5, AND PART OF THE ROAD ALLOWANCE BETWEEN LOT 22 AND 23, CONCESSION 5, (CLOSED BY BY-LAW 855, INST NO. HU8243) GEOGRAPHIC TOWNSHIP OF HUMBERSTONE) THE CITY OF WELLAND								
REGIONAL MUNICIPALITY OF NIAGARA								
DESIGN:	DRAWN:			planning p	SCALE	manag	rement O 1: 2000	
APPROVED	_{Date:} Februar	y 2	0,	2020 F	PROJEC		2681.00	
^{drawing n₀.} Dain City	East Subdivis	on.c	dwc]	_	PHA	SES 1-3	